# Resonators, Filters, and Custom Ceramic Components

Disruptive Technologies for Spectrum Management



### **Dielectric Laboratories Inc.**

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#### **Company Overview**

Dielectric Laboratories Inc. (DLI) is your global partner for application specific microwave and millimeterwave components serving customers in military, fiber optic, wireless, medical, transportation, semiconductor and avionics markets. With more than 30 years of experience, you can turn to DLI with confidence for your high frequency Single-Layer Capacitors, Multi-Layer Capacitors, Thin Film components, heat sinks, and custom microwave solutions.

DLI continues to introduce exciting new innovations in custom ceramic resonator and filter technologies. These new patent-protected products leverage decades of ceramic and thin film experience, creative and clever design expertise, and advanced prototyping and testing capabilities.

DLI is committed to serving you and thanks you for your business!

#### **Quality and Environmental Policy**

DLI's reputation for quality and environmental responsibility is based on a commitment to not only meet customer's requirements, but to exceed expectations. The entire organization, beginning with top management, strives to achieve excellence in designing, manufacturing and delivering capacitors and integrated thin film products for high frequency applications, while maintaining safe and healthy working conditions. Furthermore, DLI commits to achieve these goals in an environmentally responsible manner through our commitment to comply with environmental regulations and implement pollution prevention initiatives. DLI strives to continually improve the effectiveness of our Quality and Environmental Management Systems through the establishment and monitoring of objectives and targets.

DLI's quality system is certified to the ISO 9001:2000 international standards and its environmental system is certified to the ISO 14001:2000 international standards.

#### **RoHS Compliance Statement**

DLI is fully commited to offering products supporting Restriction of Hazardous Substances (RoHS) directive 2002/95/EC. All DLI dielectric formulations are RoHS compliant and the company offers a comprehensive range of ceramic components free of lead. DLI complies with the requirements of the individual customer and will maintain product offerings that meet the demand of our industry.

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#### Introduction

DLI has built its global reputation as a manufacturer of high frequency, high Q capacitors. In recent years, DLI has emerged as a comprehensive manufacturer of specialty ceramic components for high frequency applications. With over three decades of material science formulation and development, more then one hundred proprietary and/or patented ceramic formulations, and multiple recent patent filings, DLI is the pre-eminent ceramic component manufacturer in the industry. The marriage of ceramic expertise, manufacturing know-how, product quality, customer service, product customization, and clever microwave and RF design engineering sets us apart from all others in the industry. This product brochure will introduce you to the unique disruptive technologies that have become part of the new DLI.

#### What Makes DLI Unique?

DLI has leveraged its materials, processes and engineering capabilities to produce unique products to complement the imagination of the electronic and scientific communities. DLI has more then 100 proprietary ceramic formulations offering K values from as low as 4 to more then 40,000. DLI's ceramic formulations can be used to custom match the Thermal Coefficient of Expansion (TCE) to the customer's implementation.

To highlight how our engineers can design terrific new products for our customers, please consider just one of many core proprietary materials. Our 'CF' material has these features:

- Temperature stability of ±15 ppm/°C vs. typical Alumina which has a temperature stability of +120 ±30 ppm/°C; an 8x improvement.
- Miniaturization capabilities over typical Alumina or Printed Circuit board materials. Our CF offers a size reduction of 15x compared to PWB materials and more then 2x compared to Alumina.
- 'CF' does not exhibit signs of aging, having been used in our SLC and MLC Product Lines for decades.
- This material does not out-gas in a space environment because of the dense nature of the fired ceramic.

DLI gives its talented design engineers a broad set of proven materials on which to implement their revolutionary design ideas. *DLI redefines the envelope!* 

DLI reserves the right to make changes in product designs and/or pricing. Sales are subject to DLI's conditions of sale. DLI has no control over conditions of use; no warranty is made or implied as to suitability for customer's intended use. DLI shall in no event be responsible for incidental or consequential damages including, without limitation, personal injury or property damage. Please refer to our website, www.dilabs.com, for the latest revision of this catalog.



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Single Frequency Cavity Resonator Patent Pending

DLI's Cavity Resonators set a new standard for high Q resonator performance across a broad spectrum of frequencies. High Q resonators play a critical role in system noise performance, and employing this advantage is dramatically easier and less expensive than ever before. These products include extremely stable Single Frequency Cavity Resonators (SFCR), Wide-Band Tunable Ceramic Resonators, and Two-Port Resonators described in more detail on the following pages.

DLI has introduced a family of patent pending high-Q temperature stable cavity resonators. They provide an ideal solution for high performance, low-cost microwave or millimeter-wave oscillators and filters. This component has integral shielding, controlled coupling and tight frequency tolerances. Devices are available in both surface mount technology (SMT) and wire-bond forms, enabling automated assembly. The unique features of this patent pending device reduce circuit size and weight and eliminate the expense of fully shielded housings, manual assembly and manual frequency tuning.



- Fully shielded
- Surface mountable or wire-bondable
- *Q*'s up to 2000+
- Frequency ranges from 1 to > 67 GHz
- Excellent frequency stability vs. temperature
- High reliability thin film gold metallization
- Frequency tolerances as low as 0.1%

#### **Q** Comparison of Various Resonator Technologies



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A Sample of Applications:						
Systems	Circuits					
Automotive	Microwave & Millimeter-Wave Oscillators					
RADAR Ground-based Avionics/Missile Shipboard Communications Base Stations WLAN, WLL SONET/SDH	Fundamental Fixed Frequency Oscillators - Ultra-low Phase Noise (former solution: expensive DRO's and multiplied-up crystal or SAW based device with decreased performance)Narrow-Band Tunable VCO or Phase Locked Oscillators (typically ± 0.3% tuning) (former solution: varactor tuned expensive DRO)					
Military RFID ECM/ECCM/EW Tx/Rx Man Pack Radio Aerospace Intelligent Munitions	Integration of high performance Oscillators directly on the system motherboard without the expense and complexity of subassemblies, housing and labor intensive oper- ations typical of former solutions. Narrow bandwidth low loss filters (former solution: low loss SAW devices with frequency limitation and poor performance)					

Comparison of a DLI 10 GHz Single Frequency Cavity Resonator (SFCR) With Competing Technologies											
DLI SFCRDRO "Puck"Ceramic CoaxialL-CSAWBAWMicrostrip											
Frequency Range (GHz)	1 - 67+	1 ~ 40	0.5 ~ 5	~0 - 3	0.1 ~ 3	1 ~ 10	0.5 ~ 100				
<mark>Self Shielding</mark>	Yes	No	Yes	No	Yes	Yes	No				
SMT Capable	Yes	No	Yes	Difficult	Yes	Yes	Yes				
Chip & Wire Compatible	Yes	No	No	<i>Difficult</i>	Contamination Sensitive	Contamination Sensitive	Yes				
Q @ 2 GHz	→1500	<i>→15000</i>	~ 500	50~150	5~10000	1000~2000	100~200				
		All date	<mark>a belo</mark> w is fo	or a 10 GHz	resonator						
Q	$\rightarrow 2000$	<i>→10000</i>	N/A	N/A	N/A	500 ~ 1000	100 ~ 300				
X	0.17	1 (housing)	N/A	0.15	N/A	0.1	0.2				
Size (inches) V	0.2	1 (housing)	N/A	0.15	N/A	0.2	0.1				
Ż	0.06	<mark>0.5 (housing</mark> )	<i>N/A</i>	0.1	N/A	0.05	0.1				
Volume (in <sup>3</sup> )	$2x10^{-3}$	0.5	<i>N/A</i>	$\sim 2x10^{-3}$	N/A	N/A	$\sim 2x10^{-3}$				

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Single Frequency Cavity Resonator Patent Pending

	Part Identification Number										
ACR	08250	CF	1	S	Т						
Product <u>Family</u>	Resonant Frequency GGmmm Example: 08250=8.25 GHz	Material <u>Code</u> CF, CG, FS	Frequency <u>Tolerance</u> $1=\pm 0.1\%$ $2=\pm 0.2\%$ $3=\pm 0.5\%$ $4=\pm 1.0\%$ 9= special	Mounting <u>Code</u> S=Surface Mount (SMT) W=Microstrip Mount (see page 9)	<u>Package</u> T=Tape/Reel P= Waffle Pack						



The equivalent circuit of the Single Frequency Cavity Resonator (SFCR) near its lowest resonant frequency is shown at left. The lowest resonant mode is typically employed in oscillator and filter designs. The element values are shown for a 9.95 GHz SFCR. The resonant frequency is set by the parallel combination of Cp and Lp, and the finite unloaded Q by R. The series capacitance Cs connects the resonator L-C to the input pad, thus setting the coupling between the external circuit and the frequency controlling L-C resonator. The capacitance Csh is a stray capacitance between the input pad and ground. All of these network elements have excellent repeatability providing tight control over resonant frequency, coupling and input impedance. The structure also provides an integrated DC

blocking function, thus eliminating a tolerance sensitive element from the bill of materials. For wide bandwidth circuit modeling, S-Parameters are recommended. S-Parameters are available for downloading from our website (www.dilabs.com). The resonators are readily customized for frequency, coupling, Q, tunability and assembly requirements. For additional information on custom solutions see pages 14-16.

The Graph below depicts typical Single Frequency Cavity Resonator frequency stability versus temperature for DLI standard dielectric materials.



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	Measured Data from Selected Standard Resonators								
Resonant Frequency (GHz)	Temperature Coefficient of Frequency*	Coefficient of Frequency*		Dimensions L x W x T					
(6112)	<b>Typical</b> (ppm/°C)	Typical (dB)	(50 Ohms)	mm	inches				
8.20	CF Material: - 2.3	-25	250	5.3 x 5.3 x 0.8	0.21 x 0.21 x 0.03				
9.95	CF Material: - 2.3	-11	300	5.6 x 4.3 x 0.8	0.22 x 0.17 x 0.03				
12.80	CF Material: - 2.3	-7	350	3.8 x 3.6 x 0.8	0.15 x 0.14 x 0.03				
18.65	FS Material: - 7.3	< -25	400	6.1 x 5.6 x 1	0.24 x 0.22 x 0.04				

\* over the range  $-20^{\circ}$ C to  $+120^{\circ}$ C

The table above summarizes the characteristics of selected standard resonators, and below some selected simulations to illustrate the primary resonator design variables. The primary variables are frequency of resonance, cavity material dielectric constant, and length and width dimensions. The interaction of these variables is illustrated in the resonator size charts on the page 8. The loaded Q of the resonators is effected by the coupling coefficient (denoted in the tables in terms of return loss) and by material choice (dielectric constant), and by material thickness. Generally, resonators made from thick, low dielectric constant materials are capable of the highest loaded Q's. For reference, when a resonator has a coupling coefficient of 1.0 it will exhibit an excellent return loss at the resonance frequency and the unloaded Q of the resonator will be 2 times the loaded Q value. The desired level of resonator coupling varies with individual circuit requirements such as varactor frequency trimming, or transistor negative resistance value. Resonator input impedance versus frequency and coupling level are illustrated in the Smith Chart on page 16. The unloaded Q's of the cases shown range up to nearly 2000, clearly a new performance standard for a component compatible with automated assembly. In contrast to other "high Q" microwave resonators, DLI's cavity resonator is completely self contained, that is its loaded Q and resonant frequency can be directly measured using RF coplanar probe technology. Thus, ambiguities of special test fixtures and components which are not appropriate to the product realization are eliminated from part evaluation.

	Simulated Data for Selected Resonators								
Resonant Frequency	Temperature Coefficient of Frequency*	Return Loss @ Resonance	Loaded Q Modeled		nsions W x T				
(GHz)	Typical (ppm/°C)	Modeled (dB)	(50 Ohms)	mm	inches				
3.2	CG Material: 8.8	-22	290	8.1 x 8.1 x 3	0.32 x 0.32 x 0.1 2				
	CF Material: - 2.3	-12	550	8.1 x 8.1 x 3	0.36 x 0.36 x 0.12				
5.0	CG Material: 8.8	-12	360	5.1 x 5.1 x 3	0.20 x 0.20 x 0.12				
	FS Material: - 7.3	-12	1000	21.8 x 21.8 x 3.8	0.86 x 0.86 x 0.15				
24.0	CF Material: - 2.3	-12	480	2.0 x 2.0 x 1.3	0.08 x 0.08 x 0.05				
24.0	FS Material: - 7.3	-12	1000	4.6 x 4.6 x 3	0.18 x 0.18 x 0.12				
26.5	FS Material: - 7.3	-20	325	4.2 x 4.2 x 0.5	0.16 x 0.16 x 0.02				
40.0	FS Material: - 7.3	-18	445	2.7 x 2.7 x 0.5	0.10 x 0.10 x 0.02				
50.0	FS Material: - 7.3	-17	400	2.2 x 2.2 x 0.5	0.08 x 0.08 x 0.02				
67.0	FS Material: - 7.3	-12	600	1.6 x 1.6 x 1	0.06 x 0.06 x 0.04				

\* over the range  $-20^{\circ}$ C to  $+120^{\circ}$ C

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Single Frequency Cavity Resonator Patent Pending

### **Estimating Resonator Size**

The size of the Cavity Resonator is determined by the desired resonant frequency and the ceramic material selected. Generally, for a given frequency resonator, selecting material types which result in larger part size also result in higher Q resonators. Increased resonator height also enhances Q. For additional information consult the factory.

The charts on this page should be used as a guide for selecting the ceramic materials to be used and to closely estimate the resonator length dimension for a square device. Typical designs are nominally rectangular, with length to width aspect ratios of less than 1.2:1.











In Oscillators, the most important factor effecting phase noise performance is high resonator loaded Q. High Q is evidenced in the following graph by rapid phase slope (versus frequency) and in the narrow bandwidth of the input reflection coefficient data on pages 10-13.

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### **Mounting Alternatives**



The metallized Cavity Resonator offers unique miniaturization opportunities. Shown is an implementation where the active device and power supply bypass capacitors are assembled onto the resonator. The wirebond signal leads are kept short.

**Microstrip Mount** 

<b>Resonator Mounting, Interconnection and Metallization Schemes</b>								
Mounting Code			Backside Metallization	Topside Metallization				
Surface Mount	Component to Circuit	Solder - Sn/Pb or Sn [Lead free]	Nickel/Gold	Nickel/Gold				
S	Interface	Or Conductive Epo xy						
Microstrip Mount	Component to Substrate	Conductive Epoxy	Gold	-				
W	Interface							
	Input/Output Interconnect	Thermocompression - Wirebond	-	Gold				

For more information on metallization codes, see page 19



This illustration demonstrates a surface mounting technique. The first resonator is positioned with the I/O pad in view to demonstrate the alignment with the printed wire board geometry. The second illustration shows the resonator mounted in position. The third illustration shows the printed wire board geometry. A solder mask is used to control the flow of solder during assembly and insulate the input-line from shorting to the resonator ground metallization http://www.rfoe.net/ TEL:0755-83397033 FAX:0755-83376182 E-MAIL:szss20@163.com

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### 8.2 GHz Cavity Resonator



Resonant Frequency (GHz)	Temperature Coefficient of Frequency* Typical (ppm/°C)	Return Loss @ Resonance Typical (dB)	Loaded Q Typical (50 Ohms)	Din mm	eensions inches
8.20	CF Material: - 2.3	-25	250	5.3 x 5.3 x 0.8	0.21 x 0.21 x 0.03

\* over the range -20°C to +120°C





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### 9.95 GHz Cavity Resonator



Resonant Frequency	Temperature Coefficient of Frequency*	Return Loss @ Resonance	Loaded Q Typical	Dimensions				
(GHz)	Typical (ppm/°C)	Typical (dB)	(50 Ohms)	mm	inches			
9.95	CF Material: - 2.3	-11	300	5.6 x 4.3 x 0.8	0.22 x 0.17 x 0.03			
* over the range $-20^{\circ}$ C to $+120^{\circ}$ C								

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### 12.8 GHz Cavity Resonator



Resonant Frequency	Temperature Coefficient of Frequency*	Return Loss @ Resonance	Loaded Q Typical	Dimensions			
(GHz)	<b>Typical</b> (ppm/°C)	Typical (dB)	(50 Ohms)	mm	inches		
12.80	CF Material: - 2.3	-7	350	3.8 x 3.6 x 0.8	0.15 x 0.14 x 0.03		

\* over the range  $-20^{\circ}$ C to  $+120^{\circ}$ C





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### 18.65 GHz Cavity Resonator



Resonant Frequency	Temperature Coefficient of Frequency*	Return Loss @ Resonance	Loaded Q Typical	Dimensions		
(GHz)	Typical (ppm/°C)	Typical (dB)	(50 Ohms)	mm	inches	
18.65	FS Material: - 7.3	< -25	400	6.1 x 5.6 x 1	0.24 x 0.22 x 0.04	

\* over the range  $-20^{\circ}$ C to  $+120^{\circ}$ C





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### Narrow-Band Varactor Tuning of Cavity Resonators







0.0 -2.5 -10 -5.0 -15 -7.5 S21 (dB) Solid -10.0tted -12.5 -15.0 -17.5 -35 -20.0 85 9.5 10 10.5 11 11.5 12 12.5 Frequency (GHz)





Consider a ceramic cavity resonator for your next oscillator design. The inherent stability of ceramic offers excellent long term aging performance and temperature stability. High loaded Q's promise excellent phase noise performance.

S11

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The use of a 2-port resonator for voltage controlled oscillator applications is represented by the loop model of the oscillator above. Frequency adjustment or modulaton is easily accomplished by the introduction of the voltage variable phase shifter. Typical broadband resonator performance and the amplitude (solid) and phase (dotted) variation of the 2-port resonator over the 3 dB bandwidth are illustrated to the left.

The inherently shielded nature of the ceramic resonator, its small size, and ease of mounting present many interesting miniaturization possibilities.

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### Narrow-Band Tunable Resonator



Application of a 1-port resonator in a narrow-band or fixed frequency application is represented by the negative resistance model shown above.

### Wide-Band Tunable Resonator



A wideband VCO at microwave frequencies can be challenging to design for good phase noise. The relatively poor varactor Q degrades the loaded Q of the resonant circuit, an effect which increases with tuning range, thus degrading phase noise. To achieve the best phase noise from the oscillator, the resonator and coupling capacitors must be high Q, temperature stable and have tight tolerance. This minimizes excess tuning range and maximizes loaded Q.

DLI's Wide-Band Tunable Resonator, illustrated in the see-through 3-D graphic below, is a precision surface mounted thin film microstrip resonator with integrated coupling capacitors. DLI's proprietary ultra-stable, Hi-Q, Hi-K ceramics are employed to provide optimum performance in a miniature size. A simplified oscillator circuit incorporating the Wide-Band Tunable Resonator with integrated coupling capacitors Cs1 and Cs2 is shown above.

In contrast, current designs frequently employ discrete resonators and surface mount capacitor chips (MLC) to provide the coupling capacitances. The tolerances of these discrete parts cause significant variations in VCO unit to unit performance. The MLCs have lower Q's and larger, undesirable parasitic inductance than DLI's integrated thin film coupling capacitors. The lower parasitic effects of the DLI thin film integrated design reduce spurious oscillations, improve tuning characteristics and can enable higher frequency operation.



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### Designing a Custom Resonator



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# Self Bias Network

For self biased MIC GaAs Fet amplifiers, this device integrates source decoupling and user selectable bias resistance

### **Functional Applications**

- Wireless communication modules
- MIC broadband high gain RF/Microwave modules
- Bias line voltage divider and integrated decoupling capacitor



### <u>Benefits</u>

- Improves gain flatness and stability in GaAs FET amplifiers
- Simplifies assembly with one component
- Miniature size :.020" x .034" (.5mm x .86mm)

### **Equivalent Schematic Representation**



#### User wire bond to Ground to select resistance WB R1 Source R4 R3 To FET Source

Resistor Values: R1 - 200Ω R2 - 100Ω R3 - 50Ω R4 - 20Ω Nominal Capacitance:

50pF

Typical application requires 2 networks

**Recommended Mounting:** The Self Bias Network should be mounted with fully metalized side down directly on the RF ground plane for best performance

#### **Product Number Identification**



#### **Physical Characteristics**



**Typical Application** 



Custom Networks can be designed per customer specification. Please consult Factory for additional information or special requirements.

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TM Miniature Ceramic Filters XTREME-Q



- Rejection 45 dB typical
- Pass band Width <15%

#### Demonstrated capability of high frequency filter designs

- Lowpass, Highpass, and Bandpass
- Designs include:
  - Tchebyshev
  - Bessel cross-coupled responses in various topologies
  - Resonators (e.g. Ring and Dual mode)
  - Edge Coupled
  - End Coupled
  - Hair-Pin
  - Interdigitated
  - Custom Variants

#### Advantages of DLI Hi K materials for Microstrip Filters

- Temperature Stability: 8 fold improvement with CF material
- Filter size reduction: 1/15th the area of PWB materials
- High repeatability
- Reduced size & cost systems



Interdigitated

DLI Variant on Hair-Pin

Hair-Pin

			Тур	ical	Filter	Specif	fication	lS		
Center Freq FC (GHz)	Material Code	3dB Bandwidth (MHz)	Filter Type	# of Poles	Passband Insertion Loss (dB)	Low Side -40 dB Point (GHz) (1)	High Side -40 dB Point (GHz) (1)	Mounting Code (2)	Length inches (mm)	Width inches (mm)
2.14	CF	350 (16%)	Interdig	7	1.8	1.80 (3)	2.36 (3)	S	0.740 (18.8)	0.400 (10.2)
3.5	CF	165 (5%)	SDMRF	12	2.5	3.08	3.9	М	0.900 (22.9)	0.330 (8.4)
4.2	CF	250 (6%)	SDMRF	12	2.4	3.63	4.72	М	0.900 (22.9)	0.330 (8.4)
5.6	CF	410 (7%)	Edge Cpl	5	2.2	5.21	6.13	М	0.925 (23.5)	0.260 (6.6)
6	CF	<b>590</b> (10%)	SDMRF	16	3.7	5.62	6.53	М	0.700 (17.8)	0.330 (8.4)
6.5	CF	390 (6%)	SDMRF	16	2.7	5.96	7.24	М	0.700 (17.8)	0.330 (8.4)
9.7	CF	420 (4%)	End Cpl	7	2.9	9.36	10.04	М	1.500 (38.1)	0.100 (2.5)
37	FS	760 (2%)	End Cpl	3	2.2	34.83	39.67	М	0.325 (8.3)	0.100 (2.5)

Note 1 : higher rejection can be achieved with a cover.

Note 2 : see definition of mounting codes on adjacent page.

Note 3 : data shown for this filter is for -30 dB point.

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Part Number Identification							
AFL	06000	<b>B300</b>	S	Р	-XXXX		
Product	Center		Mounting				
<b>Family</b>	<u>Frequency</u>	Bandwith	<u>Code</u>	Package	Drawing #		
	GGmmm	mmm	S,W,M	T = Tape/Reel			
	Example:	B300=300MHz	(see below)	P=Tray			
	06000=6.00GHz						

Filter N	Iounting, Inter	connection and Meta	llization Sche	emes
Mounting Code			Backside Metallization	Topside Metallization
<u>Surface Mount</u> S	Component to Substrate Interface and Input/Output Interconnect	Solder - Sn/Pb or Sn [Lead free] Or Conductive Epoxy	Nickel/Gold	Nickel/Gold
Microstrip Mount M	Component to Substrate Interface	Solder - Sn/Pb or Sn [Lead free] Or Conductive Epoxy	Nickel/Gold	-
	Input/Output Interconnect	Thermocompression - Wirebond Or Ribbon Lead		Gold

### Mounting Codes and Metallization

3	Surface Mount - Conductive epoxy or solder mount.
	Nickel/Gold on the top and bottom surfaces of the device.
	Nickel Metallization: 20 micro-inches typical.
	Gold Metallization: 5 to 20 micro-inches typical.
	For solder applications gold is held to a minimum to prevent
	embrittlement in the solder system.
W	Microstrip Mount - Wirebond Interconnection - Conductive epoxy mount.
	Gold on the mounting surface and Gold on the top surface.
	Gold Metallization: 50 micro-inches minimum, 100 micro-inches typical.
Μ	Microstrip Mount - Wirebond Interconnection - Conductive epoxy or solder mount.
	Nickel/Gold on the mounting surface and Gold on the top surface.
	Nickel Metallization: 20 micro-inches typical.
	Gold Metallization Bottom Surface: 5 to 20 micro-inches typical.
	For solder applications gold is held to a minimum to prevent
	embrittlement in the solder system.
	Gold Metallization Top Surface: 50 micro-inches minimum, 100 micro-inches typ





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### 2.14 GHz Bandpass Filter

#### **Unique Features**

- 7-Pole Tchebyshev on K=23 ceramic
- Low loss: 1.8dB typical
- Temperature stable +/- 15ppm/°C
- Surface mountable
- Small size: 0.4 x 0.75 x 0.035 inches
- No tuning
- Good cost/size/performance tradeoff



2.14 GHz Bandpass Filter



The plot below illustrates filter performance repeatability in a surface mount comfiguration. Multiple devices fabricated on a single substrate, stringent material controls and precise processing enable excellent part repeatability at the lowest cost possible.



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### 5.6 GHz Bandpass Filter



DLI's engineers select from numerous filter topologies to solve your frequency management problem. Size, cost, and performance tradeoffs are considered. Whether you have a new requirement or are trying to architect a topology to fit an existing slot, consider a ceramic solution.

Classical filter topologies can yield excellent performance in a small footprint when fabricated on ceramic substrate materials. Miniaturization reaches new levels by employing DLI high-k ceramic formulations. Different techniques of placing the resonant structures are observed in the accompanying photographs. Lower frequency implementations rely on folded resonators whereas high frequency designs generally use end coupled designs. Coupling is managed to yield the desired pass band/reject band performance. The correct placement of the input/output structures manage the impedance of the structure.

Performance requirements are easily converted to an implementation with the aid of classical modeling tools. The final physical implementation is verified using electromagnetic simulators and DLI proprietary software. Design and prototype time is minimized.



#### 5.6 GHz Edge Coupled Bandpass Filter

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### 9.7 GHz Bandpass Filter

- 7-Pole End Coupled Filter
- 4% Bandwidth (400 MHz)
- Insertion Loss < 2.7dB</p>
- Manufactured on CF Material, K=23
- Small size (1.1"x0.1"x0.03")





Measured Response of Filter in Fixture



The End Coupled resonator topology employed here is well suited for low percentage bandwidths (typically in the 2~5% range) and high out of band rejection. The 9.7 GHz filter is pictured both individually and attached to a carrier, which enables screw assembly and form /fit /function substitution for a larger more costly alternative. DLI's high K material is utilized here for size and weight reduction. In a typical application conductive epoxy attachment to the floor of a channeled shield housing would be employed. With proper shielding, very high levels of rejection are possible. Approximately 70 dBc was achieved in this design. If designed for printed circuit materials the performance and repeatability would be inferior, and the filter length would be over 3 inches.



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### 37 GHz Bandpass Filter



The End Coupled resonator topology is applied to this 2% bandwidth filter. The narrow width (0.100 inches) of this filter design facilitates high isolation by enabling a below waveguide cut-off shielded housing. In a typical application conductive epoxy attachment to the floor of a channeled shield housing would be employed. Precision photolithography enables excellent unit to unit repeatability at low cost. DLI has precision measurement capability up to 67 GHz with the Vector Network Analyzer shown below. Both fixture and RF coplanar probe testing are employed, depending on the application.



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### Miniature 12 and 16 Pole Bandpass Filters

#### Symmetrical Dual Mode Resonators High selectivity

- Low Insertion Loss
- Compact size

#### High K ceramic

- Miniaturization
- Temperature stable
- Hi-Q (low loss)



3.5 GHz Dual Mode Bandpass Filter



#### **Applications for Dual Mode Resonator Bandpass Filters**

The small size, low insertion loss and the sharp cutoff of the dual mode bandpass filters make then ideal for:

- Communications Receivers RF and IF Applications
- Frequency Synthesizer and Oscillator Applications
- Instrumentation
- RADAR Applications



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#### 4.2 GHz Dual Mode Bandpass Filter



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### Ceramic Cavity Filters

- Utilizes single pole ceramic cavity resonator design
- Small Size 0.17 X 0.2 X 0.03 inches for a 10.5 GHz filter
- LO/Multiplier chains/RF pre-select/image filtering
- Patent Pending



#### **10.5 GHz Ceramic Cavity Filter**

**Ceramic Cavity Filter** 



Ceramic cavity resonator technology can be employed in conjunction with DLI's stable, high Q ceramics to create precise, small, low loss bandpass filters. Using a two port implementation, a very small robust filter can be created. Wide reject band performance without spurious modes is possible. The small, shielded nature of the ceramic cavity filter implementation makes it an ideal choice for integration in low noise receiver front ends with the antenna and pre-amplifier.

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### **Cascading of Filters**

The filtering characteristics of a series-cascading ceramic cavity resonator is demonstrated below. The single ceramic cavity resonator which contains one resonator and generates one transmission zero is introduced as the most basic building block for modular design of Bandpass filters. Higher-order Bandpass filters are designed by cascading single cavity resonators to generate the required transmission zeros. A simple example model filter is designed to validate the model and the design approach. The performance of the cavity resonator filter, especially the bandwidth ratio, is improved significantly in comparison with that of the single cavity resonator at the vicinity of center bandwidth frequency. In early designs, up to 3% relative bandwidths have been achieved.



SINGLE POLE CAVITY FILTER



#### **Cascaded Cavity Filter Performance**

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### Mounting

Two mounting techniques in common usage are designed to optimize performance of filters at microwave frequencies. Reliable connectivity is assured by selecting the correct metallization for the signal traces and mounting surfaces for the desired mounting and interconnecting technique. The metallization schemes offered support these mounting techniques. Customized metallization systems are available upon request.



The above illustration demonstrates a microstrip mounting technique. The circuit is relieved to accommodate the filter. The bottom surface of the filter is attached directly to the system ground plane using conductive epoxy. A minimum of 50 micro-inches and typically 100 micro-inches of gold are provided on the top surface to facilitate reliable wirebonding. [Cleaning of the surfaces using UV ozone etch or ultra-sonic techniques is always recommended to insure the highest quality of bonds.] Metallization codes W or M are suitable for this assembly method. If metallization code M is selected, solder attach of the part is enabled if thermal coefficients of expansion are compatible.



Surface mounting techniques typically rely on solder bond between the bottom conductor of the component and the ground conductor of the circuit. Note the use of multiple ground vias between the component and the system ground plane to insure optimal performance. The input/output signal connection can be realized using castellations and solder reflow. Nickel metallization is provided for solder attachment. A thin outer layer of gold is provided to prevent oxidation of the nickel. The gold is minimized to eliminate embrittlement in the solder joint. This metallization code is S.



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### **Defining a Custom Filter**

Type –Bandpass (BP), Lowpass (LP), Highpass (HP)	
Center Frequency, Fc (GHz)	Fc=GHz
3 dB Bandwidth (MHz)	BW3dB=MHz
Insertion Loss (IL) @ Fc (dB)	IL=(dB)
Return Loss (RL) @ Fc: dB Reference - 50 Ohms	RL=(dB)
Upper Frequency Rejection:	dB @ MHz
Lower Frequency Rejection:	dB @ MHz
Power Handling (Watts)	Power (average) =WattsPower (peak) =Watts
<b>Operating Temperature Range:</b>	$T \min = \underline{ C},  T \max = \underline{ C}$
Mounting Technique: Surface Mount (S) or Microstrip (M)	Circle one: S or M
Size (limits):	Length, Width, Thickness, circle one: inches or mm



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DLI utilizes the unique advantages offered by its proprietary ceramic formulations as the differentiator from typical RF and Microwave manufacturers. DLI will design both Duplexers and Diplexers to customer specifications. The distinction between the two is subtle, but the understanding is essential to proper design. **Duplexers** are three port devices used to separate and combine frequencies, having two filters with a common driving point covering two frequency bands. **Diplexers** are three port devices used to separate and combine frequencies, having two filters with a combine frequencies, having one filter covering all frequency bands

### **Typical Specifications**

### Features and Benefits

Frequencies from 1 to > 67 GHz
Insertion loss < 3 dB</li>
Return loss 20 dB minimum
Isolation > 50 dB

- Highly integrated SMT or wirebond formats
- Available in gold and copper metallizations
- Photolithography defined
- Accurately reproducible

Below is one example of a UMTS Duplexer. This discrete ceramic Duplexer utilizes high performance ceramic thin film materials from DLI. Thin film technology offers these types of devices with the ability to meet conflicting and challenging demands for size reduction, low insertion loss, bandwidth, as well as ideal matching conditions. In this case the DLI designed device eliminated 2 separate filters and an isolator in one-fifteenth the size of a PWB implementation with far better temperature stability.





UMTS Duplexer

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# **Bias Filter Network**

#### Designed to filter RF signals from bias and control lines from 10MHz to 40GHz

### **Functional Applications**

- Wireless communication modules
- Ideal varactor decoupling element
- High gain RF/Microwave modules
- Ideal GaAs FET gate biasing device
- MMIC multichip modules

I

requirements



**Physical Characteristics** 



Dimensions in inches (mm) L / W & T tolerance ± .001" (.0254)





### **Benefits**

- Filters noise and RF from Supplies.
- ■Reduces RF feedback through bias supplies.
- Simplifies assembly one component replaces many.
- Designed with large 4 mil wirebond pads for assembly ease.

#### **Equivalent Schematic Representation**



**Total Series Resistance:** 600 nominal

#### **Total Shunt Capacitance:** BT material - 140pF nominal

BH material - 95pF nominal

DC Ratings: Volts Max:50V I(mA) Max:10Ma

Recommended Mounting: The Bias filter Network should be mounted with fully metallized side down directly on RF ground plane for maximum isolation performance.

#### **Typical Applications**



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Typ.

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# Gain Equalizer

Used to compensate for the Gain Slope of other elements

#### **Functional Applications**

- Equalizer compensates for module Gain Slope
- Broadband communications, RADAR, phased arrays
- SONET modules to 40+ GHz

### <u>Benefits</u>

- Superior microwave performance
- Excellent repeatability

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■ Ease of assembly, reduced size and cost

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Typical Application Typical Broadband Module for Fiber Optic SONET



Excellent, repeatable microwave performance is achieved by application of precision thin film fabrication and DLI Hi-K Ceramic materials. DLI's unique design solution provides near Ideal R-C frequency response, far superior to "Stacked R-C chip" Assemblies.





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Part #	Resistor (R)	Low Frequency Insertion Loss, 50 ohm system (dB)	Equivalent Capacitance (pF)	F <sub>o</sub> (GHz)	Mounting Attachment material: S=solder E=epoxy	L	W	Т
AEQ 2199	43 Ω	-3.0	1.15	16	Е	0.028" ± .002" (.711 ± .051 mm)	0.016" ± .002" (.406 ± .051 mm )	0.007" ± .001" (.178 ± .025 mm)
AEQ 2050	30 Ω	-2.2	0.33	34	E	0.030" ± .002" (.762 ± .051 mm)	0.016" ± .002" (.406 ± .051 mm)	0.005" ± .001" (.127 ± .025 mm)
AEQ 2234	50 Ω	-3.5	0.31	32	Е	0.032" ± .002" (.813 ± .051 mm)	0.018" ± .002" (.457 ± .051 mm)	0.005" ± .001" (.127 ± .025 mm)
AEQ 3042	9Ω	-0.8	12.5	7	S	$0.040 \pm .002"$ (1.02 ± .051 mm)	0.020 ± .002" (.508 ± .051 mm)	0.006 ± .001" (.152 ± .025 mm)
AEQ 3055	20 Ω	-1.6	9.0	7	S	0.040 ± .002" (1.02 ± .051 mm)	0.020 ± .002" (.508 ± .051 mm)	0.006 ± .001" (.152 ± .025 mm)

Lp

Custom Equalizers can be designed per customer specification. Please consult Factory for additional information SUNSTAR射频通信 http://www.rfoe.net/ TEL:0755-83397033 FAX:0755-83376182 E-MAIL:szss20@163.com

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# Gain Equalizer

#### **Metallization:**

Epoxy mount (type "E"): Top side: TaN resistor, TiW, 100 μ inch Au minimum. Bottom side: TiW, 100 μ inch Au minimum. Solder mount (type "S"): Top side: TaN resistor, finish: 20 μ inch Au maximum over 30 μ inch Ni Bottom side finish: 20 μ inch Au maximum over 20 μ inch Ni

#### Die Attachment recommendations:

The gap in the microstrip line should nominally be equal to dimension "S" (see table).

#### Mounting attachment material:

"E" type are conductive epoxy only

"S" type can be solder or conductive epoxy

	Part Number Identification								
AEQ 34 R50 S T -xxxx									
Product	Minimum Loss	Resistance	Mounting						
<b>Family</b>	<u>Frequency</u>	in ohms	<u>Technique</u>	<u>Package</u>	Drawing #				
	GG in GHz	R50=50 ohms	S=solder attach	T=tape/reel					
	Ex: 34 is 34GHzE=epoxy mountP=waffle pack								

DLI's miniature Thin Film Gain Equalizers have a microwave frequency response which is so close to ideal that it can be modeled by the simple parallel R-C circuit shown on the preceding page. This is a convenient model for Spice (time domain) simulations. Other common equalizer implementations using stacked R-C chips are not accurately modeled by this circuit. For highest accuracy frequency domain simulations, S-parameters are recommended

The "stacked R-C chip" implementation, illustrated in the figure below has many issues in both design and manufacturing which lead to lower performance, and higher product cost. The equivalent circuit model below more accurately predicts the frequency response of the stacked chips. At microwave frequencies, the additional parasitic circuit elements are required. The effect of ESL, the equivalent inductance of the chip capacitor is particularly important as it causes a more peaked response as seen in the figure on the next page.









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# Gain Equalizer

DLI's gain equalizer frequency response is compared with that of an ideal R-C, and stacked R-C chips in the figure below. The stacked R-C chip model utilizes the same Rchip and Cchip values as in the ideal R-C model. The key point is that the chip component R and C values used in a stacked chip equalizer are generally not the ideal values for specifying the DLI single chip gain equalizer. The next section discusses specifying the part by frequency response parameters, or in terms of the ideal R-C values.



#### **Custom Equalizer Design Inputs:**

- Low frequency loss or resistance value
- Fo minimum loss frequency or capacitance determined using equivalent circuit model on page 32.
- Case size restrictions 50 ohm microstrip line width is a typical maximum case width objective



	Case Size (inches)	Preferred:   Maximum Length:   Maximum Width:
	Minimum Loss Frequency (GHz)	Fo GHz
	Low Frequency Loss ( <b>dB</b> ), 50 ohm system	Design Resistance (ohms) Loss(dB)
C	perating Temperature Range (C°)	Minimum Temperature: Maximum Temperature:
	Power Dissipation (mw)	
	Assembly Method (SMT or Epoxy)	Conductive Epoxy attach Solder attach Solder type
	Board Material	Material Dielectric constant Thickness

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# Multi-Layer Capacitors

<u>C04</u>	<u>C06</u>	<u>C08</u>	<u>C11</u>	<u>C17</u>	<u>C22</u>	<u>C40</u>
0.04 x 0.02	0.06 x 0.03	0.08 x 0.05	0.055 x 0.055	0.11 x 0.11	0.22 x 0.25	0.38 x 0.38
0.1 - 10 pF	0.1-47 pF	0.1 - 100 pF	0.1 - 100pF	0.1 – 1000pF	1 - 2700pF	1 - 5100pF
UL only	UL & CF	UL only	UL, CF, AH	UL, CF, AH	CF & AH	CF & AH
100V WVDC	250V WVDC	250V WVDC	250V WVDC	1000V WVDC	2500V WVDC	7200V WVDC

## **Build-to-Print Thin Film Processing**

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High Voltage Up to 2KV 0.2 thru 55 pF Extended Voltage Up to 15KV 0.1 thru 85 pF Available in non-mag	Sealed Glass 1.0 thru 250 pF Surface mount Vertical, panel & Horizontal Mount	Epoxy sealed 0.6 thru 14 pF Surface mount	Higher voltage single turn Surface or through-hole mount	Connectors & Cable Assemblies PC Plug, Straight & 90° Crimp Jack Non-magnetic only

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